ABSTRACT
In French-style doors a flipper mullion is provided to have an air tight seal to avoid heat leakage between the doors. It is attached to one of the French doors through both of the hinge members. However, due to the complexity of the current concept, the outside surface of the flipper mullion remains in a cold temperature, presenting moisture. The moisture is unacceptable for aesthetic and safety reasons. A usual solution is to use a heater inside the flipper mullion (7 to 10W). The heater increases the temperature of the outside surface, avoiding the moisture formation. It increases the complexity of the assembly and the energy consumption. A 7W flipper mullion heater power corresponds to 5 kWh/ month, which means around 4% of the total energy consumption of regular French door refrigerators.

In the present study, an attempt has been made to reduce the external condensation by changing the material and the design of flipper mullion. Variation of flipper mullion external surface temperature with change in the material and design of flipper mullion are investigated to determine the economically viable concept.

KEYWORDS: French door refrigerators, flipper mullion, external condensation, external surface temperature.

INTRODUCTION
In French-style doors, a flipper mullion is provided to ensure an air tight seal which prevents heat leakage. It is attached to one of the French door through first and second hinge members. Each of the first and second hinge elements have corresponding cam members [8]. The cam members include multiple lobes and extend above the hinge pins that define an axis of rotation for the mullion as shown in figure 1, while the mullion is not required to “divide” the compartments, French-style doors require a central sealing surface. Stationary mullion bar fixed to the refrigerator will limit the size and shape of goods capable of being placed in the compartment, as well as the accessibility to the goods.
Flipper mullion is carried by one of the two French-style doors. Typically, the mullion is caused to pivot when the door is opened or closed, with the mullion pivoting about hinge elements that allow the mullion to travel between first and second positions. Most designs include a locking mechanism, either in the form of a magnetic retaining element or a separate spring biased lock.

![Flipper mullion attached to a door](image)

**Properties of flipper mullion**

Flipper mullion cover is made of steel to stick onto gasket in which a magnetic strip is provided. Flipper mullion cover is provided to achieve a tight fit so that air leakages are avoided.

**Table 1. Properties of Steel**

<table>
<thead>
<tr>
<th>STEEL (Flipper mullion cover)</th>
<th>Properties</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ferromagnetic</td>
<td>Permeability μ [H/m]=1.26×10^-4 (Magnetic field at 0.002 T)</td>
</tr>
<tr>
<td>Thermal conductivity</td>
<td>50 W/mk to 60 W/mK</td>
</tr>
<tr>
<td>Thickness</td>
<td>0.48mm</td>
</tr>
<tr>
<td>Width of collar</td>
<td>9.3 mm</td>
</tr>
</tbody>
</table>

**Table 2. Properties of materials used for flipper mullion which is made of ABS Plastic**

<table>
<thead>
<tr>
<th>ABS (Flipper mullion)</th>
<th>Properties</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thermal conductivity</td>
<td>0.1 w/mk</td>
</tr>
<tr>
<td>Coefficient of thermal expansion(1/K)</td>
<td>0.00008</td>
</tr>
<tr>
<td>Thickness</td>
<td>2.54mm</td>
</tr>
<tr>
<td>Height of guider</td>
<td>10.4 mm</td>
</tr>
</tbody>
</table>

**Table 3. An insulation made of EPS**

<table>
<thead>
<tr>
<th>Insulation</th>
<th>Properties</th>
</tr>
</thead>
<tbody>
<tr>
<td>Density</td>
<td>40 kg/m³</td>
</tr>
<tr>
<td>Thermal conductivity</td>
<td>0.04 W/mK</td>
</tr>
<tr>
<td>Thickness</td>
<td>19 mm</td>
</tr>
<tr>
<td>Height</td>
<td>987 mm</td>
</tr>
</tbody>
</table>

**PROBLEM STATEMENT**

**Condensation on flipper mullion**

The flipper mullion is used in order to close the gap between the doors and avoid air leakage. However, due to the complexity of the current concept, the outside surface of the flipper mullion remains in a cold temperature, presenting moisture. The moisture is unacceptable for aesthetic and safety reasons.

![Condensation on flipper mullion](image)
The fig 3 shows two issues being faced:

i. External condensation at the flipper mullion surface and
ii. External condensation at the gasket.

The condensation at the mullion surface is caused by the heat transfer through the plastic cover and EPS part. The condensation at the gasket occurs because of the internal air flow direction, which is supplied directly to the lateral sides of the mullion.

A usual solution is to use a heater inside the flipper mullion (7 to 10W). The heater increases the temperature of the outside surface, avoiding the moisture formation. It increases the complexity of the assembly and increase the energy consumption. A 7W power corresponds to 5 kWh/month, which means around 4% of the total energy consumption of a regular French door refrigerator.

OBJECTIVES
1. Improve aesthetics by ensuring no moisture formation.
2. Suggesting improvements to remove condensation and reduce heat leaks.
3. Reduction in power consumption by removal of mullion heater thus reducing the load on compressor.
4. Suggesting improved insulation of flipper mullion by analyzing various alternative available materials.

LITERATURE SURVEY
Thermal insulations
Insulations means using some materials as thermal insulation for reducing the heat transfer in the construction of insulated body. Thermal insulation will help to reduce unwanted heat loss and can decrease the energy demands of heating and cooling system. The effectiveness of insulation is commonly evaluated by the key property of a thermal insulation material—thermal conductivity k (W/m-K), which refers to a material’s ability to conduct heat. As good insulation materials, it is needed to achieve as low thermal conductivity as possible, which enables, accordingly, a high thermal resistance as well as a low thermal transmittance.

Moreover, common insulation materials are characterized by light weight, small apparent density, loose and porous, which can barrier the thermal conductivity by the internal non-flow air. Among these, the inorganic insulation materials have non-flammability, a wide temperature range, good resistance to chemical corrosion while the organic materials have high intensity, low water absorption as well as good impermeability.

Rice husk has insulation
S. R. Bello, and T.A. Adegbulugbe [2] , they made a Comparative Study on Utilization of Rice husk alone Charcoal and Sawdust as an insulation material and reported that rice husk has better insulating properties in terms radiation and conduction losses with respective time.

Comparison of the insulation materials
This below table has presented a survey of different thermal insulation materials components. With the knowledge of the basic heat transfer mechanisms and the ways to reduce the total thermal conductivity of a material or component, novel thermal insulation materials and components were described. Thermal conductivity is a property of a substance and characterise its ability to transfer heat by conduction. In general,
the numerical value of thermal conductivity is highest for solids, the lowest for gases and it has intermediate values for liquids. A summary of the thermal Conductivity of the materials is presented.

<table>
<thead>
<tr>
<th>Materials</th>
<th>Thermal conductivity (milliW/mK) at 10 °C</th>
<th>Density (kg/m³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Jute</td>
<td>35</td>
<td>50</td>
</tr>
<tr>
<td>sugarcane fiber</td>
<td>50</td>
<td>100</td>
</tr>
<tr>
<td>coconut fiber</td>
<td>55</td>
<td>50</td>
</tr>
<tr>
<td>Rice husk</td>
<td>22</td>
<td>400-600</td>
</tr>
</tbody>
</table>

### Mathematical Modeling and Simulation Results

#### Determination of surface temperature of flipper mullion

Assuming one dimensional heat flow through flipper mullion, the major modes of heat transfer are conduction and convention. The existing mullion is compared with two prototypes with varying insulation materials and different configurations. Surfaces temperatures obtained while using these are estimated assuming a one dimensional flow of heat. The resistances offered to transfer of heat through flipper mullion is represented in Fig 5. The conditions in ambient are (generally reported values) 305K, Relative humidity 85%, Convective heat transfer coefficient $h = 9$ W/m²·K. The conditions inside the Refrigerator chamber are 278K, convective heat transfer coefficient $h = 5$ W/m²·K. As flipper mullion is a composite slab $R_{mullion}$ varies with prototypes.

![Fig: 5 Mullion as a one dimensional slab](image)

**Case 1:**
This is an existing composition of Flipper mullion. Steel, Eps and Plastic (ABS) are different materials used in Flipper mullion. $R_{mullion}$ for this prototype is shown Fig along with convective resistances.

![Fig: 6 Block diagram of flipper Mullion with EPS insulation](image)
Fig: 7 Resistance circuit of existing Flipper Mullion

The various resistances as referred to heat flow diagram are,

Table 5. List of resistances (case1)

<table>
<thead>
<tr>
<th>R_A</th>
<th>Ambient convection</th>
<th>R_7</th>
<th>Plastic under steel edge</th>
</tr>
</thead>
<tbody>
<tr>
<td>R_1</td>
<td>Plastic</td>
<td>R_8</td>
<td>Steel left</td>
</tr>
<tr>
<td>R_2</td>
<td>Steel surface</td>
<td>R_9</td>
<td>EPS Insulation</td>
</tr>
<tr>
<td>R_3</td>
<td>Plastic right side small edge</td>
<td>R_10</td>
<td>Plastic right side</td>
</tr>
<tr>
<td>R_4</td>
<td>Plastic left side small edge</td>
<td>R_11</td>
<td>EPS inside</td>
</tr>
<tr>
<td>R_5</td>
<td>Plastic under steel edge</td>
<td>R_12</td>
<td>Plastic surface</td>
</tr>
<tr>
<td>R_6</td>
<td>Steel right side edge</td>
<td>R_B</td>
<td>RC Convection</td>
</tr>
</tbody>
</table>

Case 2:

Fig: 8 Block diagram of Plastic strip Flipper Mullion Prototype

Fig: 9 Resistance circuit of plastic strip mullion
### Table 6. List of resistances (case 2)

<table>
<thead>
<tr>
<th>RA</th>
<th>Ambient convection</th>
<th>R7</th>
<th>Plastic under steel edge</th>
</tr>
</thead>
<tbody>
<tr>
<td>R1</td>
<td>Plastic</td>
<td>R8</td>
<td>Steel left</td>
</tr>
<tr>
<td>R2</td>
<td>Plastic strip</td>
<td>R9</td>
<td>EPS Insulation</td>
</tr>
<tr>
<td>R3</td>
<td>Plastic right side small edge</td>
<td>R10</td>
<td>Plastic right side</td>
</tr>
<tr>
<td>R4</td>
<td>Plastic left side small edge</td>
<td>R11</td>
<td>EPS inside</td>
</tr>
<tr>
<td>R5</td>
<td>Plastic under steel edge</td>
<td>R12</td>
<td>Plastic surface</td>
</tr>
<tr>
<td>R6</td>
<td>Steel right side edge</td>
<td>R14</td>
<td>Steel surface</td>
</tr>
</tbody>
</table>

### Case 3:

![Fig: 10 Block diagram of plastic Coating steel](image)

**Fig: 10 Block diagram of plastic Coating steel**

![Fig: 11 Resistance circuit of plastic coated filler mullion](image)

**Fig: 11 Resistance circuit of plastic coated filler mullion**

### Table 7. List of resistances (case 3)

<table>
<thead>
<tr>
<th>RA</th>
<th>Ambient convection</th>
<th>R7</th>
<th>Plastic under steel edge</th>
</tr>
</thead>
<tbody>
<tr>
<td>R1</td>
<td>Plastic</td>
<td>R8</td>
<td>Steel left</td>
</tr>
<tr>
<td>R2</td>
<td>Steel surface</td>
<td>R9</td>
<td>EPS Insulation</td>
</tr>
<tr>
<td>R3</td>
<td>Plastic right side small edge</td>
<td>R10</td>
<td>Plastic right side</td>
</tr>
<tr>
<td>R4</td>
<td>Plastic left side small edge</td>
<td>R11</td>
<td>EPS inside</td>
</tr>
<tr>
<td>R5</td>
<td>Plastic under steel edge</td>
<td>R12</td>
<td>Plastic surface</td>
</tr>
<tr>
<td>R6</td>
<td>Steel right side edge</td>
<td>R13</td>
<td>Plastic sheet over the steel</td>
</tr>
</tbody>
</table>
Problem Implementation

A matlab code is developed to determine the surface temperature for all the three cases. Flow chart describing solution procedure is shown in fig 12. Inputs to the code include ambient conditions, thermal conductivity, heat transfer coefficient and dimensions. Output of code includes surface temperature, total resistance of mullion and rate of heat transfer.

```
function [SURFACE_TIME, RCotal, Q] = total(k, R, Rb, Sa, Sb)

Rb = (k(3)) + R(5);
R = (k(1)) + R(3);
Rb = (k(3) + Rb(1) + R(5) + R(3))/R(3);
RCotal = (k(1) + Rb(1) + R(5) + R(3))/R(3);
RCotal = k(2) + Rb(1) + R(5) + R(3))/R(3);
R = (Rb(1) + R(5) + R(3))/R(3);
R = (k(3) + Rb(1) + R(5) + R(3))/R(3);
R = (k(3) + Rb(1) + R(5) + R(3))/R(3);
R = (k(3) + Rb(1) + R(5) + R(3))/R(3);
R = (k(3) + Rb(1) + R(5) + R(3))/R(3);
R = (k(3) + Rb(1) + R(5) + R(3))/R(3);
R = (k(3) + Rb(1) + R(5) + R(3))/R(3);
end
```

Fig : 12 MATLAB Code for Surface Temperature

Simulation results and discussion

Table 8. Surface temperature in different cases

<table>
<thead>
<tr>
<th>Cases</th>
<th>Surface temperature k</th>
<th>R total</th>
<th>Heat transfer Q (W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Case 1</td>
<td>297.3</td>
<td>12.88</td>
<td>2.252</td>
</tr>
<tr>
<td>Case 2</td>
<td>299.8</td>
<td>19.23</td>
<td>1.508</td>
</tr>
<tr>
<td>Case 3 (0.25 mm)</td>
<td>299.8</td>
<td>19.26</td>
<td>1.506</td>
</tr>
<tr>
<td>Case 3 (0.5 mm)</td>
<td>299.9</td>
<td>19.29</td>
<td>1.503</td>
</tr>
<tr>
<td>Case 3 (1 mm)</td>
<td>299.9</td>
<td>19.36</td>
<td>1.496</td>
</tr>
<tr>
<td>Case 3 (2 mm)</td>
<td>299.9</td>
<td>19.49</td>
<td>1.488</td>
</tr>
<tr>
<td>Case 3 (3 mm)</td>
<td>299.9</td>
<td>19.62</td>
<td>1.478</td>
</tr>
<tr>
<td>Case 3 (5 mm)</td>
<td>300</td>
<td>19.87</td>
<td>1.459</td>
</tr>
</tbody>
</table>
Conclusion:
It is observed that surface temperature increases with the thickness of the sheet. But increasing thickness reduces the pull force of the gasket and the temperatures are found to be lower than the dew point temperature.

Observation from the above results:
1. If EPS is used, the surface temperature is found to be less than dew point temperature.
2. Even with better insulation materials like aerogel, VIP, silica, glass bubbles also results in temperature lower than dew point temperature 302 K of mullion in case 1 by changing the plastics.

**EXPERIMENTAL ESTIMATION OF SURFACE TEMPERATURE**

**Condensation test**
The air gaps are present at the top and bottom of mullion. Six experiments are conducted with EPS insulation in three configurations with air gaps and closed air gaps. Temperatures along the vertical length of mullion are estimated by mounting thermocouples at respective locations. Similar six experiments are done with Rice husk as insulation material replacing EPS maintaining assumed ambient conditions in a chamber. 12 tests have been carried out in chamber and the results are presented in table 9.

**Results of obtained Surface temperature on mullion**
Table 9. Experimental Results of condensation test

<table>
<thead>
<tr>
<th>S/No</th>
<th>Part</th>
<th>Insulation material</th>
<th>Top and bottom gaps (open/closed)</th>
<th>Temperature</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>Top</td>
<td>Mid</td>
</tr>
<tr>
<td>1</td>
<td>Existing</td>
<td>EPS</td>
<td>Open</td>
<td>26.57</td>
</tr>
<tr>
<td>2</td>
<td>Plastic</td>
<td>EPS</td>
<td>Open</td>
<td>26.41</td>
</tr>
<tr>
<td>3</td>
<td>Strip</td>
<td>EPS</td>
<td>Open</td>
<td>22.15</td>
</tr>
<tr>
<td>4</td>
<td>Existing</td>
<td>EPS</td>
<td>Closed</td>
<td>26.57</td>
</tr>
<tr>
<td>5</td>
<td>Plastic</td>
<td>EPS</td>
<td>Closed</td>
<td>25.63</td>
</tr>
<tr>
<td>6</td>
<td>Strip</td>
<td>EPS</td>
<td>Closed</td>
<td>20.62</td>
</tr>
<tr>
<td>7</td>
<td>Existing</td>
<td>Rice husk</td>
<td>Open</td>
<td>21.29</td>
</tr>
<tr>
<td>8</td>
<td>Plastic</td>
<td>Rice husk</td>
<td>Open</td>
<td>20.89</td>
</tr>
<tr>
<td>9</td>
<td>Strip</td>
<td>Rice husk</td>
<td>Open</td>
<td>21.28</td>
</tr>
<tr>
<td>10</td>
<td>Existing</td>
<td>Rice husk</td>
<td>Closed</td>
<td>22.25</td>
</tr>
<tr>
<td>11</td>
<td>Plastic</td>
<td>Rice husk</td>
<td>Closed</td>
<td>20.79</td>
</tr>
<tr>
<td>12</td>
<td>Strip</td>
<td>Rice husk</td>
<td>Closed</td>
<td>21.29</td>
</tr>
</tbody>
</table>

Maximum surface temperature to avoid condensation is 302.85 K, which is the dew point temperature at an ambient temperature of 305 K and 80% relative humidity. From the numerical investigation, it is found that external surface temperature of flipper mullion is 297 K (Case 1). Surface temperature obtained after modifying the design and insulation material as described in Case 2 is found to be 299.56 K.

CONCLUSION
1. Maximum surface temperature to avoid condensation is 302.85 K, which is the dew point temperature at an ambient temperature of 305 K and 80% relative humidity. From the numerical investigation, it is found that external surface temperature of flipper mullion is 297 K (Case 1).
2. Surface temperature obtained after modifying the design and insulation material as described in Case 2 is found to be 299.56 K.
3. Core thermal conductivity makes highest effect, external surface temperature is found to be higher than the dew point temperature when Aerogel is used as insulation.
4. Rice husk with proper processing in terms of particle diameter and density can be a viable alternative.

Scope for future work
1. In the current design, air gaps are present at the top and bottom edges which significantly affect the outer surface temperature and they can be closed using plastic flap.
2. Analysis can be done after including the plastic flaps to study their affect on outer surface temperature.
3. Further analysis can be done by increasing the flipper mullion thickness to check whether the outer surface temperature is above dew point temperature.
ACKNOWLEDGEMENTS

I write this acknowledgement with great honor, pride and pleasure to pay my respects to all who enabled me either directly or indirectly in reaching this stage.

REFERENCES